



INTEGRATED SOLUTION FOR HOE BASED HOLOGRAPHIC PRINTER

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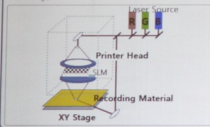
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Holographic Printer Development Goal

- Compact printer size, convenient for the consumer electronics by using WGH
- Printing speed increasing
- Low power consumption
- User convenient printing process

3D Holographic Printer

- Conventional Holo-Printer
- CE Holo-Printer



① Printer Size reduction

- Integrate conventional optical elements by WGH and replace conventional optical elements

② Printing speed-up

- Multi-hogel/head array optical architecture
- Low vibration sensitivity of the system
- High sensitive Holographic Material

③ Low Power consumption

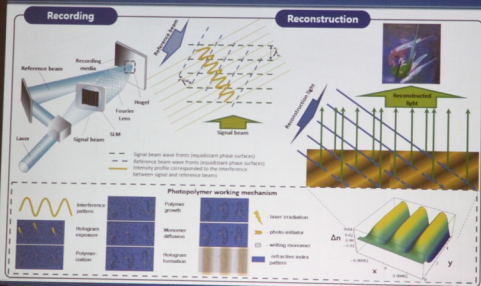
- Increase total efficiency of the optical system
- Use LD as coherent light source

④ User convenient printer process

- Film type printing material
- Dry and fast post processing

WGH Wave Guide Hologram

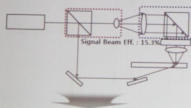
Principle of Holographic 3D Printer



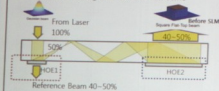
Minimization of Optical Head with WGH

- Size reduction : 10 times reduction of optical system using waveguide hologram
- Efficiency improvement by utilizing HOE (theoretically ~100%)

- Conventional Element: Volume~350cm³



- Waveguide Hologram: Volume~21.6cm³



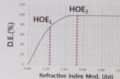
- Replace 6 conventional optical elements by 2 HOEs
 - Beam Splitter, Lens (Beam Expansion) → HOE1 (Input)
 - Lens, Mirror, Flat-Top Filter → HOE2 (Output)

[Radius of Grating for Lens]

$$r_g = \sqrt{n \lambda f + \frac{n^2 \lambda^2}{4}}$$

[Efficiency for HOE]

$$\eta = \tanh^2 \left(\frac{\pi \Delta n d}{\lambda \cos \alpha_2} \right)$$



- High optical efficiency by WGH

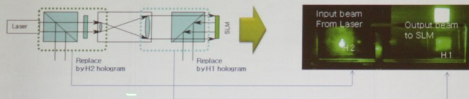
$$E_{\text{Signal}} = (1 - R)^2 \cdot T_{10}^{(2+D)} \cdot R_{10}^{2m} \cdot DE_{H1} \cdot DE_{H2}$$

Glass Transmittance(T~0.999) DE of HOE(2)

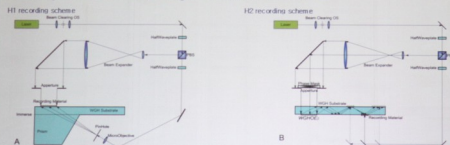
Glass Reflectance(R~4%) IR Reflectance(0.99) DE of HOE(1)~0.4

- Geometrically slim form factor benefit by using WGH
 - Folding the optical path within waveguide

Waveguide Hologram Unit Development



- Recording scheme of H1 & H2 hologram (record H1 first, then H2)

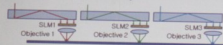


Integrate Full Color Head

Development of the compact optical printing head for full color printer

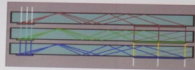
- Full color optical head requires special color cross-talk minimization system

For side by side type color system



- Optical system is complicated
- (need 3 SLM, 3 objective lens)
- Printing time increase by 3 times (vs. mono color)
- No cross-talk

Cross-talk for stacked color system



For stacked color system

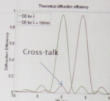


- Simple optical system (same as mono-color)
- Printing time is the same as mono-color
- Cross-talk might be an issue

$$\eta = \frac{\sin^{-1} \left(\frac{r^2 + \rho^2}{r^2 + 1} \right)}{\frac{r^2}{r^2 + 1}}$$

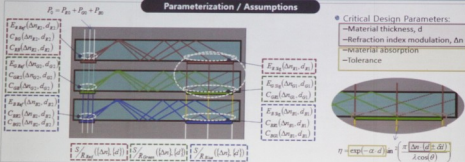
$$\xi = \frac{\pi d}{\lambda} \Delta\theta - \frac{\pi d}{2 R \lambda^2 \cos(\theta)} \Delta\lambda$$

Define cross-talk for different wavelengths



RGB Cross-talk Minimization for WGH

Parameterization / Assumptions



Mathematical Formulation

Maximization Parameters: Efficiencies

$$\begin{matrix} E_{R_{WR}}(\Delta n_{R1}, d_{R1}) & E_{R_{WG}}(\Delta n_{R1}, d_{R1}) \\ E_{G_{WR}}(\Delta n_{G1}, d_{G1}) & E_{G_{WG}}(\Delta n_{G1}, d_{G1}) \\ E_{B_{WR}}(\Delta n_{B1}, d_{B1}) & E_{B_{WG}}(\Delta n_{B1}, d_{B1}) \end{matrix}$$

Maximization Parameters: (inverse of) RGB Cross-talks

$$\begin{matrix} C_{R1}(\Delta n_{R1}, d_{R1}) & C_{R2}(\Delta n_{R1}, d_{R1}) & C_{R3}(\Delta n_{R1}, d_{R1}) \\ C_{G1}(\Delta n_{G1}, d_{G1}) & C_{G2}(\Delta n_{G1}, d_{G1}) & C_{G3}(\Delta n_{G1}, d_{G1}) \\ C_{B1}(\Delta n_{B1}, d_{B1}) & C_{B2}(\Delta n_{B1}, d_{B1}) & C_{B3}(\Delta n_{B1}, d_{B1}) \end{matrix}$$

Fixed Condition Parameters

$$\begin{matrix} S_{WR} / R_{WR}(\{\Delta n_i, d_i\}) & S_{WG} / R_{WR}(\{\Delta n_i, d_i\}) \\ S_{WR} / R_{WR}(\{\Delta n_i, d_i\}) \end{matrix}$$

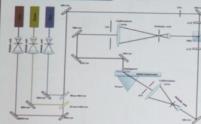
Min-Max problem is

$$\max_{\{\Delta n_i, d_i\}} \{E_{WR}(\Delta n_{R1}, d_{R1}, \Delta n_{G2}, d_{G2}, \Delta n_{B3}, d_{B3}, \Delta n_{R2}, d_{R2}, \Delta n_{G1}, d_{G1}, \Delta n_{B2}, d_{B2}, \Delta n_{R3}, d_{R3}, \Delta n_{G3}, d_{G3}, \Delta n_{B1}, d_{B1})\} = \sum_{i=1}^{11} f_i(\{\Delta n_i, d_i\})$$

For Film type (thickness fixed), it reduces to: $\max_{\{\Delta n_i\}} \{E_{WR}(\Delta n_{R1}, \Delta n_{G2}, \Delta n_{B3}, \Delta n_{R2}, \Delta n_{G1}, \Delta n_{B2}, \Delta n_{R3}, \Delta n_{G3}, \Delta n_{B1})\} = \sum_{i=1}^{11} f_i(\{\Delta n_i\})$

RGB WGH Experimental Results

Recording Scheme



Samples

Recorded WGHs



Stacked RGB WGHs

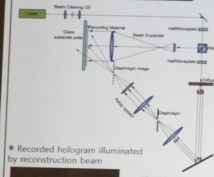


Crosstalk test results

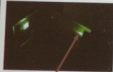
		w/o beam shaping	With beam shaping
Red	on Green	1%<	1%<
	on Blue	1%<	1%<
Green	on Red	1%<	1%<
	on Blue	1%<	1%<
Blue	on Red	1%<	1%<
	on Green	1%<	1%<

Full Integrated Printer Head

Reference Arm Recording scheme



- Recorded hologram illuminated by reconstruction beam



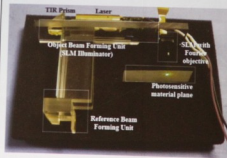
Formed hologram spot

Direct hologram view



Integrated Head

- The fully integrated optical printing head
 - WGH based beam splitting
 - WGH with integrated Phase Mask to make flat-top beam transformation and hologram shaping
 - HOE based reference beam forming unit
 - Solid design to provide low vibration sensitivity
 - LD as coherent light source



Printed Hologram Results

- All Samples were printed with recorded RGB WGH units
- The RGB hogels were recorded simultaneously for all colors
- The samples were directly recorded on Bayer Photopolymer material

